

4. PAVLENKO A.L. and APIKYAN ZH.G., Supersonic flow around a stiff wedge by a linearly elastic medium, *Izv. Akad. Nauk UzbekSSR, Ser. Tekh. Nauk*, 2, 1969.
5. BORZYKH A.A. and CHEREPANOV G.P., On the theory of the fracture of solids subjected to powerful electron beam pulses, *PMM*, 44, 6, 1980.
6. BORZYKH A.A., A spatial selfsimilar problem on the supersonic cleavage of an elastic body, *PMM*, 45, 2, 1981.
7. BYKOVYSEV G.I., KOLOKOL'CHIKOV A.V. and SYRGUNOV P.N., Selfsimilar solutions of the equations of the dynamics of an ideal elastic plastic body under Trescaplasticity conditions, *Prikl. Mekhan. Tekh. Fiz.*, 6, 1984.
8. BYKOVYSEV A.S., Propagation of complex discontinuities with piecewise-constant and variable velocities along curvilinear and branching trajectories, *PMM*, 50, 5, 1986.
9. BYKOVYSEV A.S., Modelling of fracture processes occurring in the focal zone of a tectonic earthquake, *Proc. Intern. Conf. on Computational Mechanics*, 1, Pt.3. Springer-Verlag, Berlin, 1986.
10. MADARIAGA R., The dynamic field of Haskell's rectangular dislocation fault model, *Bull. Seismol. Soc. Amer.*, 68, 4, 1978.
11. BYKOVYSEV A.S., On wave fields produced by propagating dislocation discontinuities, *Experimental Seismology in Uzbekistan*, Fan, Tashkent, 1983.
12. BYKOVYSEV A.S. and KRAMAROVSKY D.B., The displacement field produced by the propagating rectangular rupture plane: The exact three-dimensional solution, *Proc. Intern. Conf. on Computational Mech.*, 2, 6, Springer-Verlag, Berlin, 1986.
13. BYKOVYSEV A.S. and KRAMAROVSKII D.B., On the propagation of a complex fracture area, *Exact three-dimensional solution*, *PMM*, 51, 1, 1987.
14. CAGNIARD L., *Reflection and Refraction of Progressive Seismic Waves*, McGraw-Hill, New York, 1962.
15. ABRAMOWITZ M. and STIGAN I.M., Eds. *Handbook on Special Functions with Formulas, Graphs and Mathematical Tables*, Nauka, Moscow, 1979.

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MOMENT THEORY OF ELECTROMAGNETIC EFFECTS IN ANISOTROPIC SOLIDS*

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A moment (polar) theory of deformable solids is constructed for anisotropic media such as polarizable piezoelectric ceramics. The linear theory is considered in detail and an explanation of the non-linear change in the electric field inside a polarized piezoelectric material (the Mead effect) is given. The classical theory of electromagnetic effects in solids does not enable certain observed effects to be described (for example, the Mead effect /1/). Attempts to eliminate this drawback of classical theory /2, 3/ rest on the introduction of the polarization gradient into the enthalpy as a parameter of the process. Models of complex media which takes into account the internal mechanical and electromagnetic moments have been constructed in electrodynamics (for example /4, 5/) when electromagnetic fields interact with the medium. Below, a solution of the problem is given and an example of a natural description of the Mead effect is presented.

Suppose $x^i (i = 1, 2, 3)$ is a Lagrange system of coordinates frozen into a medium which occupies a volume V with a boundary S . The vector $\mathbf{r}(x^i, t)$, defines the position of a point of this medium with respect to a fixed inertial system y^i , where t is the time. The vector $\mathbf{r}^* = \mathbf{r} + \mathbf{u}(x^i, t)$ defines the position of material points of the medium after strain, where \mathbf{u} is the displacement vector. Further constructions which are carried out have the purpose of

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describing the behaviour of piezoelectric ceramic media which are brittle, and naturally, cannot be subjected to appreciable strain or bending. For this reason the further constructions are carried out in a geometrically linear formulation. For small displacements, Green's strain tensor has covariant components

$$E = \varepsilon_{ik} r_i^k, \quad 2\varepsilon_{ik} = \nabla_i u_k + \nabla_k u_i = r_i \cdot \partial u / \partial x^k + r_k \cdot \partial u / \partial x^i$$

while the Cauchy stress tensor has contravariant components σ^{ik} . The stress vector on an area with unit vector $n = n^i r_i$ is

$$P_n = \sigma^{ik} r_k n_i; \quad \Sigma = \sigma^{ik} r_i r_k \neq \sigma^{ik} r_k r_i \quad (1)$$

while the vector of the internal moment on the same area is

$$\mu_n = \mu^{ik} n_i r_k; \quad M = \mu^{ik} r_i r_k \neq \mu^{ik} r_k r_i \quad (2)$$

where μ^{ik} are the components of the moment tensor. It follows from the equations of equilibrium for the forces and moments for an elementary volume that

$$\nabla_i \sigma^{ik} + Q^k = 0, \quad \nabla_i \mu^{ij} + c^{ijk} \sigma_{ik} + \mu^i = 0 \quad (3)$$

where $Q^i r_i$, $\mu^i r_i$ are vectors referred to unit volume of the mass forces and moments. It follows from (3) that in general $\sigma^{ik} \neq \sigma^{ki}$.

We will use the condition that for an arbitrary volume of the body the sum of the second-order moments $[r \times [r \times F]]$ with respect to an internal point is in equilibrium. We then obtain the equality $\mu^{ik} = \mu^{ki}$, which will henceforth be assumed to be satisfied.

The sum of the work done by the external forces and moments

$$\delta A = \int Q \cdot \delta u \, dV + \int P_n \cdot \delta u \, dS + \int \mu \cdot \delta \omega \, dV + \int \mu_n \cdot \delta \omega \, dS$$

where ω is the rotation vector, and, taking expressions (1) and (2) into account, this can be converted to the form

$$\delta A = \int \sigma^{ik} \delta \varepsilon_{ik} \, dV + \int \mu^{ik} \delta \xi_{ik} \, dV + \int v^i \delta \gamma_i \, dV$$

Here

$$\begin{aligned} 2\varepsilon^{ik} &= \sigma^{ik} + \sigma^{ki}, & 2v^j &= c^{jik} l_{ik}, & 2l^{ik} &= \sigma^{ik} - \sigma^{ki} \\ 2\varepsilon_{ik} &= \nabla_i u_k + \nabla_k u_i, & 2\xi_{ik} &= \nabla_i \omega_k + \nabla_k \omega_i, & 2\eta_{ik} &= \nabla_i u_k - \nabla_k u_i \\ & & 2\gamma^j &= c^{jik} \eta_{ik} - \omega^j \end{aligned}$$

In this notation, Eqs. (3) take the form

$$\nabla_i l^{ik} - c^{ikj} \nabla_i \nabla_m \mu_m^j = c^{ikj} \nabla_i \mu_j - Q^k \quad (4)$$

$$v^j = -\nabla_i \mu^{ij} - \mu^j \quad (5)$$

Above and everywhere henceforth integration is carried out over the volume V and the surface S .

The increment of energy of the electromagnetic field in the volume V and the amount of heat dissipated due to the fluxes q_h and q_e of the magnetic field H and the electric field E can be expressed as follows (B and D are the magnetic and electric induction and I is the current strength):

$$\delta W = \int q_h^i \delta E_i \, dS + \int q_e^i \delta H_i \, dS = \delta \int (E \cdot D' + H \cdot B') \, dV + \delta \int E \cdot I \, dV \quad (6)$$

where the right-hand side is taken as the energy by definition /6/.

By adding to the middle and right-hand sides the terms

$$-\int n_j c^{kj} H_i \delta E_k \, dS + \int n_j c^{jik} E_i \delta H_k \, dS$$

we obtain

$$\begin{aligned} & \int (q_h^k - n_j c^{jik} H_i) \delta E_k \, dS + \int (q_e^k + n_j c^{jik} E_i) \delta H_k \, dS = \\ & \int (D'^k + I^k - c^{jik} \nabla_j H_i) \delta E_k \, dV + \int (B'^k + c^{jik} \nabla_j E_i) \delta H_k \, dV \end{aligned} \quad (7)$$

When Maxwell's equations are satisfied the right-hand side of the last equation is zero and, consequently, for arbitrary variations δE_k and δH_k , the boundary conditions for the fluxes q_h and q_e follow from (7). Hence, relations (6) and (7) are analogues of Lagrange's variational equation, written for an electromagnetic field.

Including in our considerations the inflow of heat due to the flux vector of its q through the surface S and due to internal sources of intensity r , we obtain the following equation for the increment of the internal energy of the medium:

$$dU = \delta A + \delta W + \left(\int r dV \right) dt - \left(\int q \cdot n dS \right) dt \quad (8)$$

The total amount of heat absorbed by the body in a time dt is

$$\delta Q = \left(- \int q \cdot n dS + \int r dV + \int E \cdot I dV + \int W' dV \right) dt$$

where W' is the rate of generation of heat due to conversion of mechanical energy and the energy of the interaction of the electromagnetic and mechanical fields into heat. Using Gauss's theorem for the rate s' of increase of entropy per unit volume, we obtain (T is the absolute temperature)

$$Ts' = - \nabla_i q^i + r + \sigma, \quad \sigma = E \cdot I + W' \quad (9)$$

In view of the fact that $q_i \nabla^i T \leq 0$ and $\sigma \geq 0$ for irreversible processes, the Clausius-Duhem inequality

$$s' + \nabla_i (q^i/T) - r/T \geq 0$$

follows from (9).

Introducing the free energy $F = u - Ts$ we obtain from (8)

$$F' = t^{ik} \dot{\epsilon}_{ik} + \mu^{ik} \dot{\xi}_{ik} + v^i \dot{\gamma}_i + E^i D_i + H^i B_i - sT' - W'$$

$$W' = \sum W_{\chi^A} \dot{\chi}^A$$

where χ^A are additional parameters of the process with a generalized tensor index A , and W_{χ^A} are generalized forces corresponding to them.

Further constructions depend on the choice of the parameters χ^A and the functions W_{χ^A} . If, for example $\epsilon_{ij(n)}$, $\xi_{ij(n)}$, $\gamma_{i(n)}$ are the irreversible components of the strains, in which t_{ik} , μ_{ik} , v_i perform work which is dissipated in the form of heat with powers

$$t^{ij} \dot{\epsilon}_{ij(n)} \geq 0, \quad \mu^{ij} \dot{\xi}_{ij(n)} \geq 0, \quad v^i \dot{\gamma}_{i(n)} \geq 0$$

then, using the notation

$$\dot{\epsilon}_{ij(e)} = \dot{\epsilon}_{ij} - \dot{\epsilon}_{ij(n)}, \quad \dot{\xi}_{ij(e)} = \dot{\xi}_{ij} - \dot{\xi}_{ij(n)}, \quad \dot{\gamma}_{i(e)} = \dot{\gamma}_i - \dot{\gamma}_{i(n)} \quad (10)$$

we obtain from the expression for F'

$$t^{ij} = \partial F / \partial \dot{\epsilon}_{ij(e)}, \quad \mu^{ij} = \partial F / \partial \dot{\xi}_{ij(e)}, \quad v^j = \partial F / \partial \dot{\gamma}_{j(e)} \quad (11)$$

$$E^k = \partial F / \partial D_k, \quad H^k = \partial F / \partial B_k, \quad s = -\partial F / \partial T$$

It is obvious that $\dot{\epsilon}_{ij(e)}$, $\dot{\xi}_{ij(e)}$, $\dot{\gamma}_{i(e)}$ is the rate of increase of elastic (locally irreversible) strains, while the first three groups of Eqs. (11) represent generalizations of Green's formulas, which are well-known in the theory of elasticity, to the case of inelastic strains. Similar generalizations are possible for the groups of formulas (11) for E_k and H_k , if irreversible parts of the increments of the quantities D_i and B_i can exist. For χ^A we must introduce evolution equations [7]. Replacing s' in (9) by its expression

$$s' = -d(\partial F / \partial T) / dt$$

which follows from (11), we obtain an equation for the heat flux.

We will further assume that $I = 0$, which occurs in dielectrics, and we will assume that the deformation process is reversible over the range of variation of the parameters of the process considered.

For crystals of the class (6mm) /8/ with one axis of mechanical and electrical symmetry, for which we take the x_3 axis of a Cartesian system of coordinates $x_1 x_2 x_3$, the number of fundamental parameters of the process will include the scalars ϵ_{33} , ξ_{33} , D_3 , B_3 , γ_3 , T , the vectors $\epsilon_{\alpha 3}$, $\xi_{\alpha 3}$, D_α , B_α , γ_α , and the tensors $\epsilon_{\alpha\beta}$, $\xi_{\alpha\beta}$ ($\alpha, \beta = 1, 2$).

We will introduce the following limits. Suppose the process is isothermal and the effect

of the magnetic field is small. This is the case in dielectrics. Moreover, we will assume that $\gamma_3 \simeq 0$, $\gamma_\alpha \simeq 0$ (similar to Kirchoff's hypotheses in the theory of thin plates). In this case, the quantities v^i are found from conditions (5) after solving Eq.(4), which reduces to three equations with three required functions $u_i(x_k, t)$. In addition we will assume that $W = 0$. With these limitations, the arguments of the function F will be

$$\varepsilon_{33}, \xi_{33}, D_3; \varepsilon_{\alpha 3} e^{\alpha 3}, \xi_{\alpha 3} \xi^{\alpha 3}, D_\alpha D^\alpha; e_\alpha^\alpha, \varepsilon_{\alpha\beta} e^{\alpha\beta}, \varepsilon_{3\alpha} e^{\alpha\beta} e_{\beta 3}; \quad (12)$$

$$\xi_\alpha^\alpha, \xi_{\alpha\beta} \xi^{\alpha\beta}, \xi_{\alpha 3} \xi^{\alpha\beta} \xi_{\beta 3}$$

and the mixed (combined) invariants will be

$$\varepsilon_{3\alpha} D^\alpha, \xi_{3\alpha} D^\alpha, \xi_{\alpha 3} e^{\alpha 3}, \xi_{\alpha\beta} e^{\alpha\beta}, \varepsilon_{3\alpha} e^{\alpha\beta} \xi_{\beta 3}, \xi_{3\alpha} \xi^{\alpha\beta} e_{\beta 3}, \dots \quad (13)$$

which represent the mutual orientation of the tensors and vectors occurring in them. Of the mixed invariants (13) in the number of arguments of the function F we can only include those of them that satisfy the condition that all the set of arguments of the number (12) and (13) are independent. For example, the set of components ε_{ik} , ξ_{ik} , D_i contains 15 parameters. Hence, to the twelve basic arguments (12) we can additionally add not more than three invariants from (13), whereas the remaining ones will be numerically dependent on the previously chosen independent fifteen.

The defining relations (11) and the system of arguments (12) and (13) introduced, which can be generalized in a natural way to crystals with lower symmetry, enable us to construct fairly general forms of relations between the fields, taking into account the physical non-linearity and the effect of the temperature.

In order to demonstrate the possibility of describing the Mead effect within the framework of the relations constructed, we will introduce a number of simplifying assumptions. Suppose the fields ε_{ik} and ξ_{ik} are weakly coupled. Of the invariants (13) we need then only retain the first two. Taking this into account and retaining only the second powers in the expansion for F in powers of the main parameters, and taking into account the unstressed nature of the initial state, we obtain the defining relations (11) in the form

$$\begin{aligned} t_{11} &= c_{11}e_{11} + c_{12}e_{22} + c_{13}e_{33} - e_{31}D_3, \quad t_{22} = c_{12}e_{11} + c_{11}e_{22} + c_{13}e_{33} - \\ &\quad - e_{31}D_3, \quad t_{33} = c_{13}e_{11} + c_{13}e_{22} + c_{33}e_{33} - e_{33}D_3 \\ t_{13} &= 2c_{44}e_{13} - e_{15}D_1, \quad t_{23} = 2c_{44}e_{23} - e_{15}D_2 \\ t_{12} &= 2c_{66}e_{12} = (c_{11} - c_{22})e_{12} \\ E_1 &= -e_{15}e_{13} - d_{15}\xi_{13} + \lambda_1 D_1, \quad E_2 = -e_{15}e_{23} - d_{15}\xi_{23} + \lambda_1 D_1, \\ E_3 &= -e_{31}e_{11} - e_{31}e_{22} - e_{33}e_{33} - f_{31}(\xi_{11} + \xi_{22}) - f_{33}\xi_{33} + \lambda_3 D_3 \end{aligned} \quad (14)$$

(the relations for μ_{ik} are obtained from the relations for t_{ik} by replacing ε_{ik} , c_{ik} , e_{ik} by ξ_{ik} , d_{ik} , f_{ik} respectively).

The relations for t_{ik} and E_i , ignoring terms with ξ_{ik} , repeat those usually employed (/8-11/ etc.).

For the kinematic characteristics we have (the unwritten relations are obtained by cyclic permutation of the indices 1, 2, 3)

$$\begin{aligned} \varepsilon_{11} &= \frac{\partial u_1}{\partial x_1}, \quad 2\varepsilon_{12} = \frac{\partial u_2}{\partial x_1} + \frac{\partial u_1}{\partial x_2} \\ \xi_{11} &= \frac{\partial}{\partial x_1} \left(\frac{\partial u_3}{\partial x_2} - \frac{\partial u_2}{\partial x_3} \right), \quad 2\xi_{12} = \frac{\partial}{\partial x_1} \left(\frac{\partial u_1}{\partial x_3} - \frac{\partial u_3}{\partial x_1} \right) + \frac{\partial}{\partial x_2} \left(\frac{\partial u_3}{\partial x_2} - \frac{\partial u_2}{\partial x_3} \right) \end{aligned}$$

We will consider a piezoelectric ceramic element of thickness $2h$ along the x_1 axis, when the element is polarized in the direction of the x_3 axis. An external electrostatic field with vector $E = E_1 e_1$ acts on the specimen. Then, over the whole crystal $t_{11} = t_{22} = t_{33} = 0$, $D_3 = D_2 = 0$ and, consequently, $\varepsilon_{11} = \varepsilon_{22} = \varepsilon_{33} = 0$. Since only the additional moments $\mu_2 = \alpha E_1$ operate due to the action of the field E_1 on the dipoles oriented along the x_3 axis, we have $\varepsilon_{12} = 0$, $\varepsilon_{23} = 0$, $2\varepsilon_{13} = \partial u_3 / \partial x_1$ when $u_1 = 0$, $u_3 = u_3(x_1)$. In addition, $\xi_{11} = \xi_{22} = \xi_{33} = 0$, $2\xi_{12} = -\partial^2 u_3 / \partial x_1^2$. Together with this we have

$$\begin{aligned} t_{13} &= c_{44}dw/dx - e_{15}D_1, \quad \mu_{13} = -D_1 d_{15}, \quad \mu_{23} = 0 \\ \mu_{12} &= -1/2 (d_{11} - d_{22})d^2 w / dx^2 \quad (w = u_3, x = x_1) \end{aligned}$$

Eq.(4) for $k = 3$ can be written in the following form:

$$2d^2 w / dx^2 - (d_{11} - d_{22})d^4 w / dx^4 + \alpha dE_1 / dx = 0 \quad (15)$$

Moreover, by (14) we have

$$2E_1 = -e_{15}dw/dx + 2\lambda_1 D_1 \quad (16)$$

In the polarized crystal considered, due to the action of the external electric field E_{1e}

there will be uncompensated charges at the boundaries $x = \pm h$, whereas inside the charge density will be zero. Hence, in view of Maxwell's equation for the divergence of the induction it follows that $D_{1d} = \text{const}$ inside the dielectric when $-h < x < h$. Eliminating the electric field E_{1d} in the dielectric from Eqs. (15) and (16) we obtain a uniform equation, the solution of which is

$$w(x) = A \operatorname{sh} \omega x + B \operatorname{ch} \omega x + Cx + D$$

$$\omega^2 = (d_{11} - d_{22}) / (2c_{11} - \alpha e_{15})$$

In view of the conditions of the problem, the function $w(x)$ is skew symmetric with respect to x and, consequently, $B = D = 0$. At the boundaries $x = \pm h$ we have $t_{13} = 0$, and elimination of the rigid rotation by the condition $dw/dx = 0$ when $x = 0$ gives

$$C = -\omega A, \quad A = e_{15} E_1 / [c_{44} \omega (\operatorname{ch} \omega h - 1)] \quad (17)$$

Since, on passing through the boundary of the dielectric, the induction D_1 should retain its value, while in a vacuum $D_{1e} = E_{1e}$, and whereas in a dielectric, together with (16), we must have $D_{1d} = E_{1d} + 4\pi P$, where P is the polarization, which in the case considered, according to (16), is represented by the term with dw/dx , we have $\lambda_1 = 1$. Hence, in the dielectric the electric field is given by the equation

$$E_{1d} = E_1 - e_{15} A \omega (\operatorname{ch} \omega x - 1) / 2$$

where A is given by the second equation of (17). Hence, the electric field inside the dielectric is non-linearly variable, which leads to the Mead effect. When $E_1 = 0$, $E_2 = 0$, $E_3 \neq 0$ this effect should not be observed in the type of crystals considered.

When constructing a non-linear theory, in general we must include the invariants (12) and (13) in the number of arguments of the function F . By taking into account the non-linearity connected with the dissipation of energy, we ensure an appropriate form of the function or the functional W , in which it is also possible to take into account the dissipation of the energy of the electromagnetic field itself and its interaction with the medium using models such as Maxwell's, Voigt's Boltzmann-Volterra etc.

To describe the Mead effect in crystals which are unpolarized from the beginning, but are polarized due to an external electric field, we must introduce the tensor $\nabla_i D_j$ as the argument of the function F in (11) and consider the system of defining relations (14) by extending the system of invariants (12) and (13).

REFERENCES

1. MEAD C.A., Electron transport in thin insulating films, Proc. Intern. Symp. on Basis Problem in thin Film Physics. Göttingen: Vandenhoeck and Ruprecht, 1966.
2. MINDLIN R.D., Polarization gradient in elastic dielectrics, Intern. J. Solids and Struct. 4, 6, 1968.
3. MINDLIN R.D., Continuum and lattice theories of influence of electromechanical coupling on capacitance of thin dielectric films, Intern. J. Solids and Struct. 5, 11, 1969.
4. SEDOV L.I. and TSYPKIN A.G., The construction of models of continuous media interacting with an electromagnetic field, PMM, 43, 3, 1979.
5. ZHELNOROVICH V.A., The equations for liquids with internal magnetic and mechanical moments, Izv. Akad. Nauk SSSR, MZhG, 5, 1974.
6. ILYUSHIN A.A., The Mechanics of a Continuous Medium, Izd. MGU, Moscow, 1978.
7. KOLAROV D., BALTOV A. and BONCHEVA N., The Mechanics of Plastic Media, Mir, Moscow, 1979.
8. BERMINKUR D., KERRAN D. and SHAFFE G., Piezoceramic and Piezomagnetic Materials, Physical Acoustics, 1. Pt. A. Methods and Device of Ultrasonic Research, Mir, Moscow, 1966.
9. NOVATSKII V., Electromagnetic Effects in Solids, Mir, Moscow, 1986.
10. GETMAN I.P. and USTINOV YU.A., The theory of non-uniform electroelastic plates, PMM, 43, 5, 1979.
11. GETMAN I.P., RYABOV A.P. and USTINOV YU.A., The possibilities of the method of averaging in the problem of the propagation of waves in an electromagnetic elastic layer with a periodic non-uniformity over the thickness, Izv. Akad. Nauk. MTT, 3, 1987.

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